

# High-energy 1064-nm pumped optical parametric oscillator for the 6 $\mu\text{m}$ spectral range based on $\text{HgGa}_2\text{S}_4$

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**Abstract:** The defect chalcopyrite crystal  $\text{HgGa}_2\text{S}_4$  has been employed in a 1064-nm pumped optical parametric oscillator to generate <7 ns long idler pulses near 6.3  $\mu\text{m}$  with energies as high as 3 mJ, tunable in a broad spectral range from 4.5 to 9  $\mu\text{m}$ .

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## 1. Introduction

Defect chalcopyrites with chemical formula  $\text{A}^{\text{II}}\text{B}^{\text{III}}\text{C}^{\text{VI}}_4$  and point group  $\bar{4}$  symmetry exhibit substantially higher second order nonlinear susceptibility compared to their chalcopyrite analogues, especially having in mind the close band-gap values, but in fact only one such ternary crystal, mercury thiogallate  $\text{HgGa}_2\text{S}_4$  (HGS), and the quaternary  $\text{Cd,Hg}_{1-x}\text{Ga}_x\text{S}_4$  (a solid solution of mercury and cadmium thiogallates) have been used so far for phase-matched nonlinear frequency conversion [1]. All the properties, frequency conversion experiments and the existing literature on these nonlinear crystals have been reviewed in [1]. The most important advantage of HGS over the commercially available chalcopyrite  $\text{AgGaS}_2$  (AGS, the standard non-oxide mid-IR material when it comes to pumping down-conversion schemes near 1  $\mu\text{m}$ ) is the  $\sim 1.8$  times higher nonlinear coefficient  $d_{36}$  of HGS and this at slightly increased band-gap value (2.79 eV for HGS against 2.7 eV for AGS), i.e. at somewhat improved damage resistivity [2]. In fact, the effective nonlinearity of HGS can be even higher but at present, the unknown relative sign of the  $d_{36}$  and  $d_{31}$  tensor components does not allow one to utilize both of them by optimizing the azimuthal angle  $\varphi$  [1].

Due to its wide band-gap, HGS, similar to AGS, can be pumped near 1  $\mu\text{m}$  by short or ultrashort pulse laser sources (e.g. Nd:YAG at 1064 nm) without two-photon absorption. Only few other non-oxide crystals possess this property but most of them (the biaxial  $\text{LiGaS}_2$ ,  $\text{LiInS}_2$ ,  $\text{LiGaSe}_2$ ,  $\text{LiInSe}_2$ , and  $\text{BaGa}_4\text{S}_7$ ) exhibit nonlinear susceptibility lower than AGS. The recently developed chalcopyrite  $\text{CdSiP}_2$  (CSP) is highly nonlinear and non-critically phase-matchable crystal but its clear transparency extends only up to  $\sim 6.5$   $\mu\text{m}$ , with an optical damage threshold not better than that of AGS [2].

Recently, we demonstrated an optical parametric oscillator (OPO) based on HGS which delivered the highest idler output (6.1 mJ at 4.03  $\mu\text{m}$  or 610 mW at a repetition rate of 100 Hz) of any non-oxide nonlinear material pumped at 1064 nm [3], in fact the only millijoule class OPO based on such a wide band-gap non-oxide nonlinear crystal. The main challenge to extend these results to longer wavelengths (where oxide crystals really fail) is the decreasing parametric gain. This makes it difficult to achieve few times above threshold operation before surface damage occurs. Here we demonstrate that HGS presents a perfect combination of properties that enable such operation with type-II phase matching, reaching idler energy of 3 mJ at 6.3  $\mu\text{m}$  which is an improvement of more than 6 times compared to previous best results with  $\text{CdSiP}_2$  and  $\text{BaGa}_4\text{S}_7$  based OPOs [4,5].

## 2. Experimental set-up

The HGS element used in the present study was 10.76 mm-long with an aperture of  $\sim 9.5 \times 9.5$   $\text{mm}^2$ , and wedge of  $15''$ . It was cut at  $\theta=50.2^\circ$  and  $\varphi=0^\circ$  for type-II (eo-e) interaction utilizing only the  $d_{36}$  component of the nonlinear tensor. This results in 36% higher effective nonlinearity  $d_{\text{eff}} = d_{36} \sin 2\theta$  than type-I. The crystal faces were antireflection-coated (AR) for the signal wavelength range with a single layer of  $\text{Al}_2\text{O}_3$  centered at 1280 nm which reduced substantially the Fresnel losses also at the pump wavelength of 1064 nm, see Fig. 1a. The resulting transmission at 1280 nm was 98% and at 1064 nm it was 94%. This corresponds to absorption losses of  $\sim 2\%$ /cm at the signal and pump wavelengths and residual Fresnel reflection of  $\sim 2\%$  per surface at 1064 nm. At the idler wavelength of 6.3  $\mu\text{m}$  (normal incidence) the AR-coating had no effect on the sample transmission, however, the internal losses were about 10%/cm.

The OPO was pumped by a diode-pumped Q-switched Nd:YAG laser/amplifier system delivering up to 250 mJ per pulse at 100 Hz, as shown in Fig. 1b. The pump pulse duration was typically  $\sim 8$  ns, the bandwidth 30 GHz ( $1 \text{ cm}^{-1}$ ) and the  $M^2$  factor  $\sim 1.4$ . A mechanical shutter (S) with an aperture of 8 mm was employed to reduce the repetition rate to 10 Hz. A half-wave plate (HWP) and a polarizing beam splitter (PBS) were used to attenuate the pump beam and a telescope consisting of two AR-coated lenses with  $f_{L1}=-5$  cm and  $f_{L2}=10$  cm was applied to expand it to a diameter of 9.6 and 8.45 mm in the horizontal and vertical directions, respectively. The pump polarization was horizontal and the HGS crystal rotation axis for tuning was vertical.

The pump beam reached the HGS crystal after reflection at the ZnSe bending mirror M2 ( $R=98\%$ ) and passing through the output coupler (OC) which transmitted  $96\%$ . The ZnS OC with radius-of-curvature of  $-2$  m had a transmission of  $\sim 30\%$  for the signal wave and  $92\%$  for the idler. A plane Ag-mirror M3 was used as a total reflector for all three waves in a double pump pass singly resonant OPO configuration. The physical cavity length was  $L_{\text{OPO}}=5.2$  cm. The  $4\ \mu\text{m}$  cut-on filter (F) was used to suppress the signal and pump radiation and the  $f=20$  cm BaF<sub>2</sub> lens L3 collected the output idler radiation onto the energy meter. In the following the measured idler energy values were corrected for the transmission of M2 ( $79\%$ ), F, and L3.

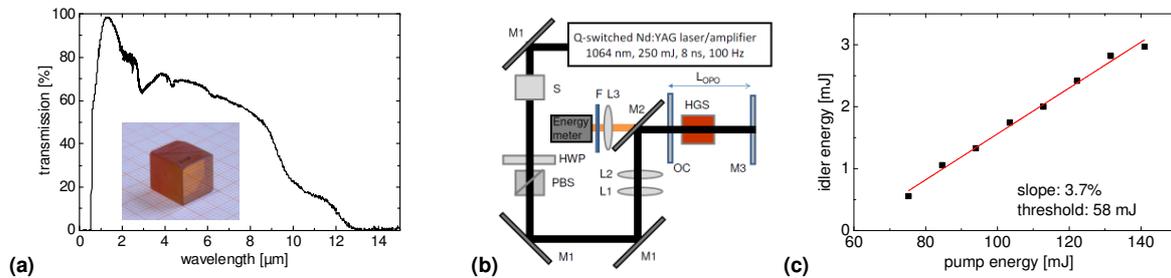


Fig 1. Transmission of the AR-coated HGS crystal with an inset showing a photograph of the OPO element (a), HGS OPO experimental set-up (b), and input-output characteristics of the OPO at normal incidence (idler wavelength of  $6300\ \text{nm}$ ) (c).

### 3. Experimental results and discussion

Figure 1c shows the input-output characteristics obtained at normal incidence. Only the idler is effectively out-coupled and measured. The threshold of  $\sim 58$  mJ corresponds to an axial pump fluence of  $0.18\ \text{J}/\text{cm}^2$  or a peak intensity of  $\sim 23\ \text{MW}/\text{cm}^2$ . This represents a substantial increase compared to the  $4\text{-}\mu\text{m}$  HGS OPO we described in [3] although type-II interaction was employed in the present case to compensate for the reduced parametric gain. The increased threshold is partly due to the longer cavity, however, shorter cavity was not advantageous with respect to achieving higher maximum idler energy because the slope efficiency was also lower. The maximum idler efficiency with the  $5.2$  cm long cavity (Fig. 1c) reached  $2.1\%$  which is equivalent to a quantum conversion efficiency of  $12.5\%$ , the slope being equal to  $21.9\%$ .

The maximum pump level of  $\sim 55\ \text{MW}/\text{cm}^2$  axial intensity applied in Fig. 1c was considered to be safe concerning surface damage to the nonlinear crystal because preliminary tests on uncoated and AR-coated plates of HGS revealed a damage threshold of  $200\text{-}250\ \text{MW}/\text{cm}^2$ . However, formation of scattering centers which affect the crystal transmission was detected when the crystal was used in the OPO cavity which was a cumulative irreversible effect depending strongly on the repetition rate and pump level. This was the reason to adopt a repetition rate of  $10\ \text{Hz}$  in the present study instead of the  $100\ \text{Hz}$  available from the commercial pump source. Hence, development of such bulk damage (which, when reaching the surface, can lead to fatal surface damage) should be related to the high intracavity signal intensity and could be possibly suppressed in future experiments by further decreasing the OC reflectivity at the signal wavelength. The highest idler energy of  $3\ \text{mJ}$  obtained with the  $5.2$  cm long cavity (Fig. 1c), corresponds to an improvement of more than 6 times compared to previous best results with CdSiP<sub>2</sub> and BaGa<sub>4</sub>S<sub>7</sub> based OPOs [4,5] and represents the highest idler energy ever demonstrated above  $6\ \mu\text{m}$  with a  $1\text{-}\mu\text{m}$  pumped OPO based on a non-oxide material. It is known that highest conversion efficiencies are achieved at higher ratios of the pump energy to the threshold, however, with the present OPO it was impossible to reach operation 3-times above threshold without bulk damage to the OPO crystal or damage of the Ag total reflector. Higher efficiency and idler energies could be, however, possible using a top-hat shaped pump beam profile which requires a special beam converter. At maximum pump level, the pump depletion measured in the present OPO was about  $22.5\%$ , roughly  $10\%$  higher than the maximum quantum conversion efficiency. Since no parasitic nonlinear losses were detected for the pump, the difference can be attributed to intracavity losses at the idler wavelength (reflection, absorption, scattering) which are not taken into account when calculating the quantum efficiency from the idler output energy. Although both depletion and conversion efficiency started to saturate from a pump energy of  $\sim 130$  mJ and linear increase of the output energy is expected further, higher conversion efficiency could be achieved with optimized pump, cavity and crystal parameters.

Close to the OPO threshold we measured at normal incidence a signal wavelength of  $\sim 1280\ \text{nm}$ , accordingly the idler wavelength is  $6.3\ \mu\text{m}$ . Figure 2a shows a comparison of the experimental OPO tuning with calculations based on the Sellmeier equations for HGS that gave the best agreement [6]. Even not far above threshold the idler tuning range extended from  $\sim 4.5$  to above  $9\ \mu\text{m}$ . The energy dependence in Fig. 2b is in agreement with the parametric gain defined by  $d_{\text{eff}}$  and the interacting wavelengths. The “anomalous” peak at normal incidence is due to enhanced

feedback for the idler wave. In fact this feedback made it possible that the OPO operated without OC: this regime was, however, less efficient and tuning was impossible since the feedback worked only at normal incidence.

We measured the HGS OPO linewidth at the signal wavelength using a 1-mm-thick Ag-coated CaF<sub>2</sub> Fabry-Perot etalon and obtained  $\sim 2.3 \text{ cm}^{-1}$  or  $\sim 0.4 \text{ nm}$  at 1280 nm. Without OC this linewidth was  $\sim 5.5 \text{ cm}^{-1}$  or  $\sim 0.9 \text{ nm}$  which is much closer to the calculated spectral acceptance bandwidth of  $8.9 \text{ cm}^{-1}$  [6].

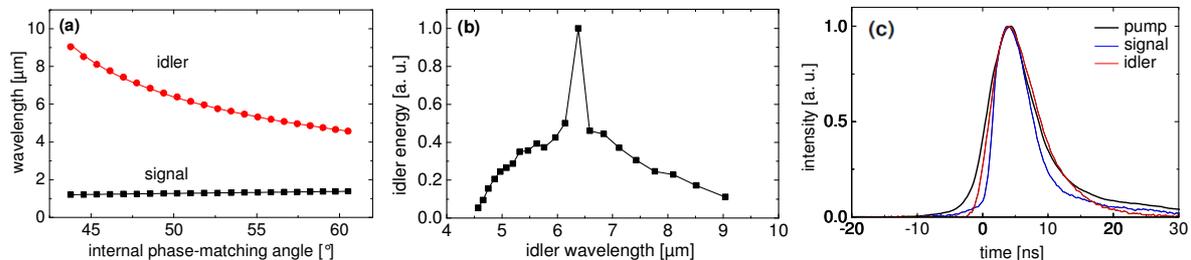


Fig. 2. Experimental signal (squares) and idler (circles) OPO wavelengths vs. internal phase-matching angle  $\theta$  compared with calculations (lines) based on Sellmeier equations [6] (a), relative idler energy vs. idler wavelength at pump energy of 80 mJ (b), and simultaneously measured temporal pulse profiles of the pump, signal, and idler (c).

The temporal characteristics of the HGS OPO were measured at pump energy of 100 mJ using fast photodiodes and 0.5 GHz oscilloscope. The (HgCdZn)Te detector used for the idler had a specified time constant of  $< 2 \text{ ns}$  at  $9 \mu\text{m}$  but clearly affected the system response at  $6.3 \mu\text{m}$ . It is obvious that both the signal ( $\sim 6.5 \text{ ns}$ ) and the idler pulses ( $< 7 \text{ ns}$ ) are shorter than the pump pulse duration, Fig. 2c.

The  $M^2$  beam quality factor of the HGS OPO was far above the value corresponding to diffraction limited beams: for the non-resonated idler, two times above threshold, we fitted data measured by the knife-edge method with  $M^2 \sim 31.5$  in the noncritical and  $M^2 \sim 28$  in the critical plane. The high  $M^2$  values can be attributed to a combination of factors including the large pump diameter and the short pump pulse duration [7]. They are, however,  $\sim 6$  times better than in our previous work [3] due to the increased cavity length and it can be expected that this parameter could be substantially improved in the future implementing the RISTRA cavity OPO concept [8].

#### 4. Conclusion

We conclude that HGS has the greatest potential of all known non-oxide nonlinear crystals that can be pumped near  $1\text{-}\mu\text{m}$  (powerful Nd- or Yb-based pulsed laser systems) for coverage of the mid-IR wavelength range up to  $\sim 12 \mu\text{m}$ . The present results indicate that energies  $> 5 \text{ mJ}$  at  $6.3 \mu\text{m}$  should be possible by better extraction of the idler wave, which includes AR-coatings for the mid-IR and reduction of the residual crystal losses. Reduction of the HGS OPO threshold by using longer crystal samples will dramatically improve the chances to avoid bulk damage formation and increase the repetition rate to 100 Hz for higher average power. The same can be achieved using flat top pump beam shaping and/or RISTRA cavity design, which has proved to be the best solution for reaching highest idler pulse energies in this mid-IR spectral range from similar OPOs pumped near  $2 \mu\text{m}$  [8].

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